

ANALYSIS AND CONTROL OF VOLTAGE HARMONICS GENERATED BY THYRISTOR CONTROLLED SERIES CAPACITORS*

A. KAZEMI**, S. M. MOUSAVI BADEJANI AND M. A. S. MASOUM

Center of Excellence for Power System Automation and Operation, Dept. of Electrical Engineering,
Iran University of Science & Technology, Tehran, I. R. of Iran
Email: kazemi@iust.ac.ir

Abstract– This paper analyzes the harmonic performance of thyristor controlled series capacitors (TCSCs) in power systems and proposes an effective method for their control and limitation in the compensated line. This is performed by proper selection of TCSC elements (capacitance and inductance) and by introducing a new method for adjusting its firing angle such that high line loadability as well as low harmonics generation is achieved. Finally, a TCSC is designed, modeled, simulated and analyzed. The main contribution is the consideration of power quality phenomena, as well as loadability in the TCSC control scheme.

Keywords – TCSC, harmonics, firing angle and loadability

1. INTRODUCTION

Thyristor controlled series capacitor (TCSC) provides continuously variable capacitance by controlling the firing angle. TCSCs have many benefits for AC transmission systems such as improved efficiency [1], controlled power flow [2], enhanced transient stability [3], improved power quality [4] and power transfer capability, as well as damping sub-synchronous resonances [5]. To achieve these advantages, proper schemes for controlling TCSC firing angles are required. Several strategies have been proposed and used for controlling TCSC in power system utilities [6].

The main drawbacks of TCSC are the nonlinear effects on system stability, discrete (non-continuous) impedance and harmonics injection. It is known that harmonic currents and the resulting harmonic voltages can be magnified considerably causing all sorts of operational problems, especially if a resonance occurs at one of the harmonic frequencies. For this reason, a recommended limit of 1% for each harmonic voltage is set and used in power systems above 138 kV [7]. In compensated transmission lines using TCSC, harmonic currents and voltages depend on the size and location of the compensator [2]. Therefore, it is important to consider the harmonic performance when designing TCSCs.

In this paper, line loadability in the presence of TCSC is presented. Voltage harmonics of TCSC versus line current as a function of its firing angle are computed and analyzed. MATLAB facilities are used to simulate a sample system with a designed TCSC. Several case studies are used to demonstrate the impact of the firing angle on overall system power quality. Finally, an adaptive control scheme is proposed for TCSC that considers conventional (e.g., loadability) and power quality issues.

2. TCSC BASIC THEORY

The basic configuration of TCSC makes use of a fixed capacitor in parallel with a thyristor controlled reactance (TCR) as shown in Fig. 1.

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**Corresponding author

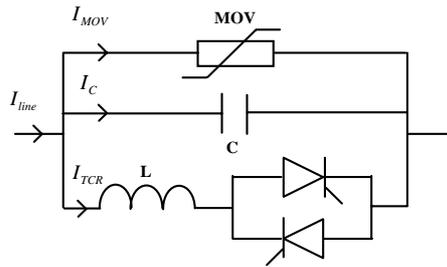


Fig. 1. Basic circuit of TCSC (C: fixed series capacitor, L: thyristor controlled inductance, MOV: Metal oxide varistor, I_{line} : line current)

In order to simulate the performance of TCSC and illustrate its effects on transmission line loadability and power quality, the 345 kV, 382 km line located in the southwest region of the United States is considered [2]. System diagram and line parameters are illustrated in Fig. 2 and Table 1. The main purpose of using TCSC is to reach the maximum power transfer (P_{Max}^{L1}) of the transmission line (e.g., 100% compensated).

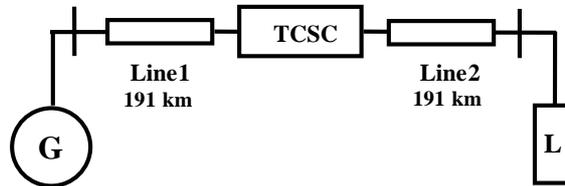


Fig. 2. The 345 kV, 382 km line (located in the southwest region of the United States [2]) used for simulations

The quotient between the resonance frequency of TCSC ($\omega_r = 1/\sqrt{LC}$) and the network frequency (ω) is

$$\lambda = \frac{\omega_r}{\omega} = \sqrt{X_C / X_L} \tag{1}$$

where X_C and X_L are bank capacitance and thyristor branch reactance, respectively. The fundamental component of TCSC voltage [8] is used to measure the equivalent device impedance

$$|X_1| \equiv \left| \frac{V_1}{I_{line}} \right| = -\frac{1}{\omega C} + \frac{K}{C\omega\pi} (\delta + \sin(\delta)) - \frac{4K \cos^2(\frac{\delta}{2})}{\omega\pi(\lambda^2 - 1)} (\lambda \tan(\lambda \frac{\delta}{2}) - \tan(\frac{\delta}{2})) \tag{2}$$

where, $K = \omega_r^2 / (\omega_r^2 - \omega^2)$.

Figure 3 shows the fundamental impedance of TCSC as a function of its firing angle α .

Table 1. Transmission line parameters for the 345 kV, 382 km line (Fig. 2) located in the southwest region of the United States [2]

z (series impedance)	$.027 + j.375$ [Ω/km]
y (shunt admittance)	$j4.273$ [$\mu/\Omega.\text{km}$]
I_C (current carrying capacity)	1050 [A]
SIL (surge impedance loading)	400 [MW]
P_{Max} (practical line loadability)	460 [MW] (≈ 1.15 pu)
P_{Max}^{L1} (thermal limit)	625 MW] (≈ 1.5 pu)
P_{Max}^{L2} (theoretical limit)	790 [MW] (≈ 2 pu)

Generally, a TCSC is controlled by varying the firing angle, measured from the zero crossing of line current or capacitor voltage waveforms. Among published papers, two definitions for the reference waveform of firing angle are presented [9-10]. The relation between α and δ (TCR conduction angle) for these cases are

$$\alpha + \frac{\delta}{2} = \pi \tag{3}$$

$$\alpha + \frac{\delta}{2} = \frac{\pi}{2} \tag{4}$$

Equations (3) and (4) are used when α is adjusted based on the capacitor voltage (e.g., measured from zero crossing of the capacitor voltage) and the line current (e.g., measured from zero crossing of the line current), respectively.

In Eq. (2), the conduction angle δ is always less than π , therefore this equation becomes infinitely large when the conduction angle is equal to δ_r (e.g., $\cos(\lambda\delta_r/2) = 0$). At this angle, resonance occurs in the TCSC and its fundamental impedance will be unlimited. For $\delta < \delta_r$ ($\alpha > \alpha_r$) fundamental impedance of TCSC (X_1) will be negative (e.g., the capacitive region in Fig. 3) and for $\delta > \delta_r$ ($\alpha < \alpha_r$), X_1 will be positive (e.g., the inductive region in Fig. 3).

Figure 4 demonstrates the electrical parameters of a TCSC in the capacitive region. The equivalent capacitor of this region is [5]

$$C(\delta) = C - \frac{\delta - \sin(\delta)}{\pi\omega^2 L} \tag{5}$$

Equation (5) illustrates the equivalent capacitive reactance of the TCSC due to the firing effect of TCR with conducting angle δ .

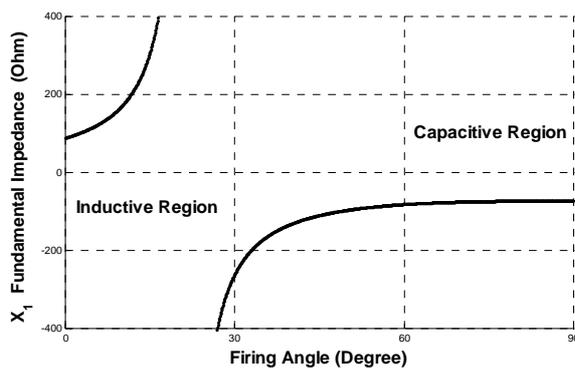


Fig. 3. Fundamental impedance of TCSC

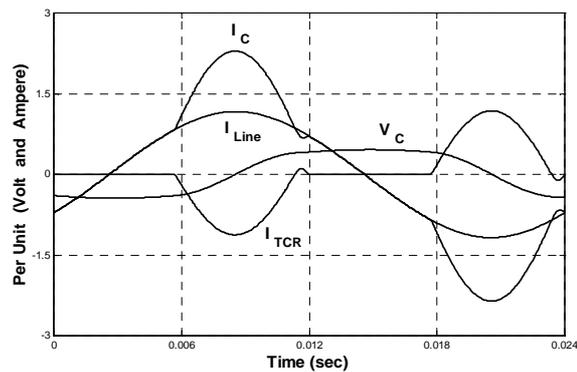


Fig. 4. Electrical parameters of TCSC

3. ANALYSIS OF TCSC HARMONICS

Following the same methodology as used in Eq. (2), for the fundamental coefficient of the TCSC voltage, the ratio of harmonic voltages to line current is

$$\left| \frac{V_n}{I_{line}} \right| = \frac{Num(\delta)}{Den(\delta)} \tag{6}$$

where

$$Num(\delta) = 4 \times \omega_r^2 \left[\cos\left(\frac{n\delta}{2}\right) \cos\left(\frac{\delta}{2}\right) \omega_r \omega (n^2 - 1) - \cos\left(\frac{n\delta}{2}\right) \sin\left(\frac{\delta}{2}\right) (n^2 \omega^2 - \omega_r^2) - \sin\left(\frac{n\delta}{2}\right) \cos\left(\frac{\delta}{2}\right) n (\omega_r^2 - \omega^2) \right]$$

and

$$Den(\delta) = nC\pi\omega(n^2 - 1)(\omega_r^2 - \omega^2)(n^2\omega^2 - \omega_r^2)$$

In Eq. (6), the ratio of harmonic voltages to line current depends on the TCSC component values [11]. To demonstrate the impact of TCSC parameters on its harmonic performance, four cases are analyzed. The main parameters of TCSC are computed for a fixed capacitance of $X_C = -73\Omega$ (e.g., 50% compensation of line impedance in TCSC blocking mode), as shown in Table 2. Fig. 5 shows plots of low order harmonic voltages amplitudes versus TCSC firing angle for these four cases.

Table 2. Computed TCSC parameter values for different cases

Case	X_L (Ohm)	λ	α_r (degree)
1	50	1.2	15.8
2	40	1.3	23.7
3	30	2	43.1
4	20	2.7	56.8

4. CONTROL OF TCSC HARMONICS

The performance of TCSC is better in the bypass mode [9] for small values of X_L . The bypass mode is utilized as a means to reduce the capacitor stress during fault conditions. In this mode it is better to have a large value for λ and small X_L (Table 2). However, from the harmonics point of view, it is better to have a large X_L (Fig. 5).

Therefore, in selecting parameter values of TCSC, one must make a compromise between its performance and loadability (Table 2) and generated harmonics (Fig. 5).

According to Fig. 5, cases 1 and 2 are better than cases 3 and 4. Also, for improving the performance of TCSC, it is better to select the smaller value of X_L [9] between these two cases. So for the system under consideration (Fig. 1), selecting $X_L = 40\Omega$ (e.g., case 2 in Table 2) is more appropriate since it generates fewer harmonics (Fig. 5b) and enjoys a relatively large value of λ .

To control and limit harmonic pollutions of TCSC without distracting its main functions, we propose an adaptive control method. This controller adapts the value of control to the system according to the operating region from a specified table. In this paper, for each region the control must consist of at least two parameters: value and sign. In this paper the value is a small deviation of firing angle. So for choosing in the first, the desired value of TCSC firing angle is set according to the conventional criteria (e.g., loadability). Then, a small deviation of firing angle ($\Delta\alpha$) is applied for power quality improvements. This is done by selecting the controller gain according to the second column of Table 3. These signs are selected based on the highest harmonics order generated by TCSC (e.g., The third harmonics of Fig. 5b). This is the worst harmonics in this study (Table 4). Note that the controller gain is constant and only affects the transient characteristics of TCSC.

Table 3. The sign of the proposed adaptive controller for different firing angle regions

α region	controller sign
0-12 [Degree]	-1
12-22 [Degree]	+1
22-38 [Degree]	-1
38-47 [Degree]	+1
47-63 [Degree]	-1
63-77 [Degree]	+1
77-90 [Degree]	-1

The maximum compensation of harmonics in this control method is limited by $\Delta\alpha$. This parameter is achieved by permissible power line changes near the desired value.

Table 4. Maximum value of TCSC Harmonics in case 4 ($\alpha=0-90$, Degree).

Harmonics order	3	5	7	9	11	13	15	17	19	21
Max ($ V_n/I_{line} $)	1.255	0.216	0.075	0.034	0.018	0.011	0.007	0.005	0.003	0.002

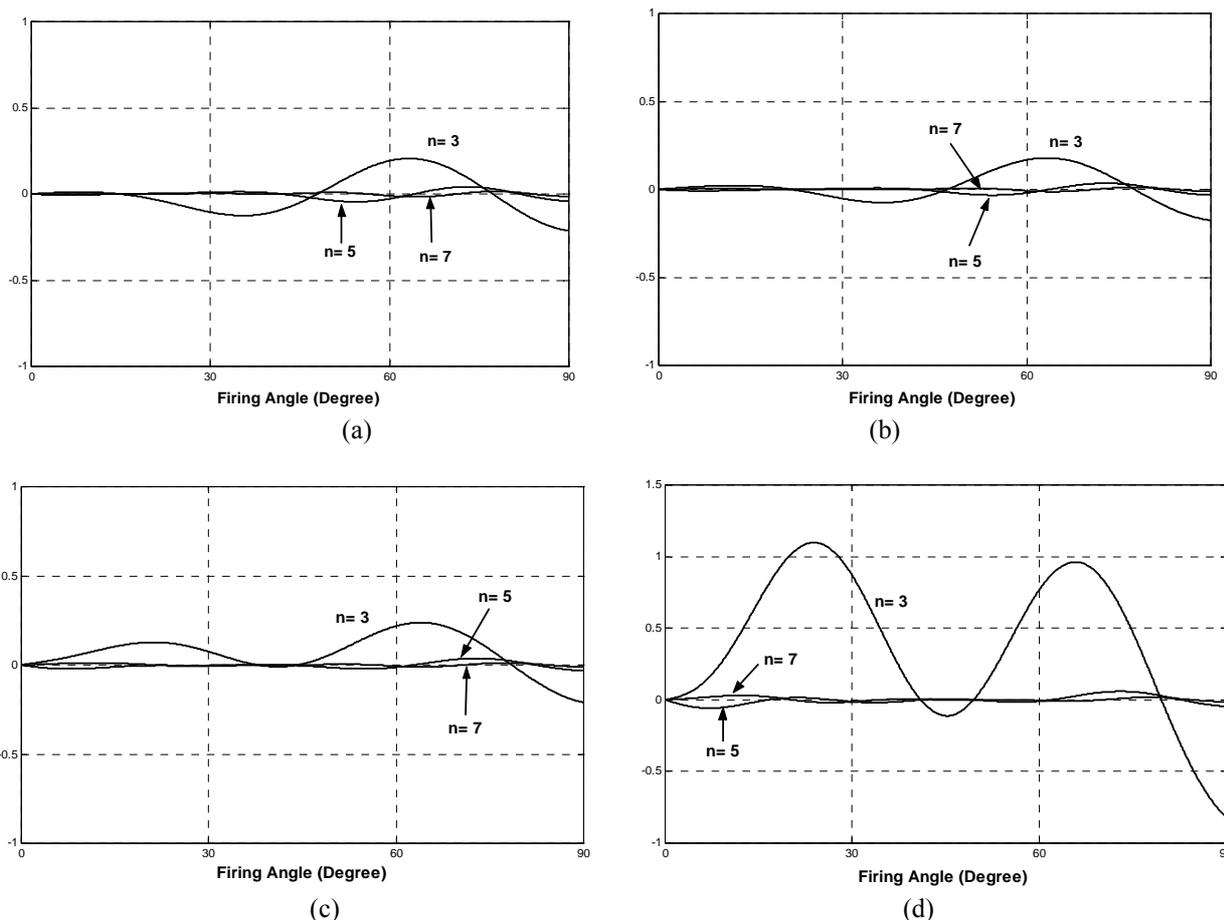


Fig. 5. Ratio of TCSC harmonic voltages to line current ($|V_n/I_{line}|$) for different values of TCSC parameters (Table 2): (a) Case 1; (b) Case 2; (c) Case 3; (d) Case 4

5. SIMULATION RESULTS

Simulink facilities are used to simulate and investigate the harmonic performance of TCSC as shown in Fig. 6. The generator is simulated using the equivalent source-impedance circuit as shown by the "Equivalent Generator" block in Fig. 6a. For simulation of transmission lines (e.g., two 191 km lines of Fig. 1), blocks, "Line 1" and "Line 2" are used. In addition, three measurement blocks are considered for monitoring the electrical parameters of the transmission lines. The main block, called "Series Comp. (TCSC)", simulates the compensation characteristic of TCSC as shown in Fig. 6b. The main part of this figure is the "Switch and Control Block", which is demonstrated in Fig. 6c.

6. ANALYSIS

In Fig.7 the electrical parameters of the transmission line are presented for different values of firing angel. At $\alpha = 0^\circ$ and 5° , TCSC operates in the inductive region. The capacitive region is obtained at firing angles of 37.8° , 60° and 90° . At 37.8° , the TCSC compensation level is 100% and the power transmitted from the line is adjusted for 1.6 per unit (e.g., the thermal limit in Table 2) as shown in Fig. 7a. The difference of Figs. 7a and 7b shows the line power dissipation. In addition, sending current and receiving voltage (per unit) are shown in Figs. 7c and 7d, respectively.

For the firing angles discussed in Fig. 7, the voltage harmonics behavior of TCSC are computed and plotted in Fig. 8. In this figure, the dominated harmonics of TCSC (e.g., the third harmonics) with and without the proposed adaptive $\Delta\alpha$ control scheme is shown.

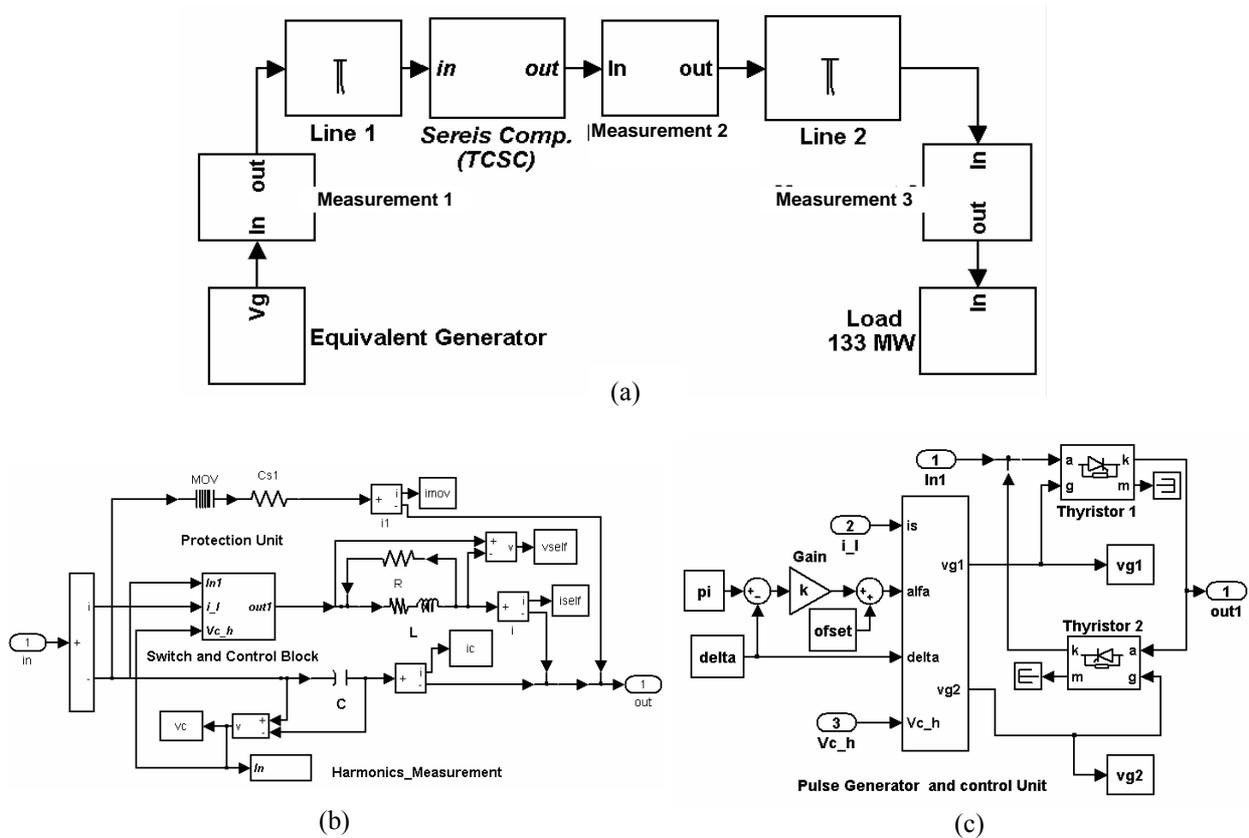


Fig. 6. Simulated TCSC system (Fig. 1) and controller: (a) system diagram; (b) details of TCSC block and protection circuit; (c) details of switching and control block

It is interesting to know that for some cases, harmonics controlling does not have any major impact on TCSC main characteristics. This is demonstrated for a selected case in Fig. 9. It is evident that firing angle control for harmonics mitigation has not affected the main functions of TCSC.

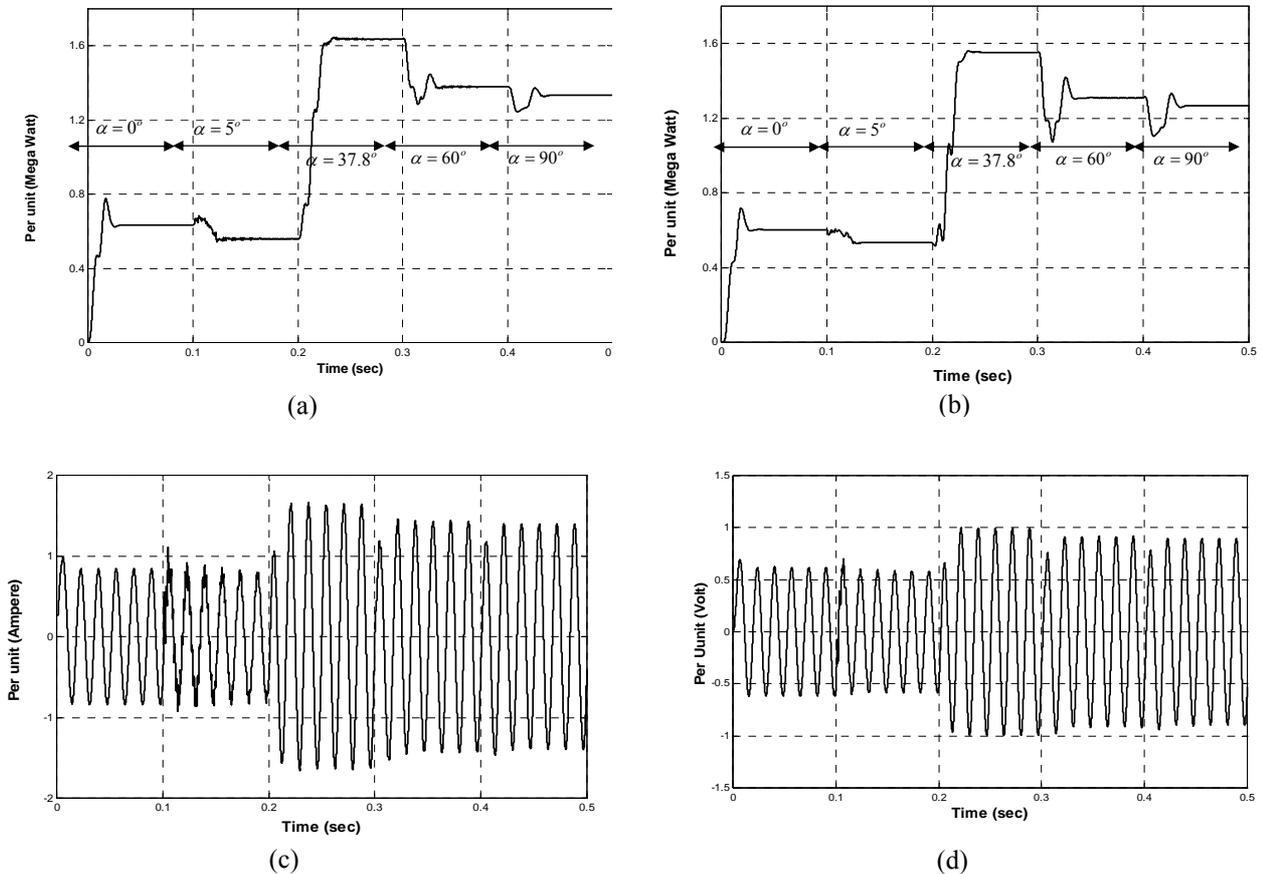


Fig. 7. Simulation results: transmission line parameters for different firing angles: (a) sending power; (b) receiving power; (c) sending current; (d) receiving voltage

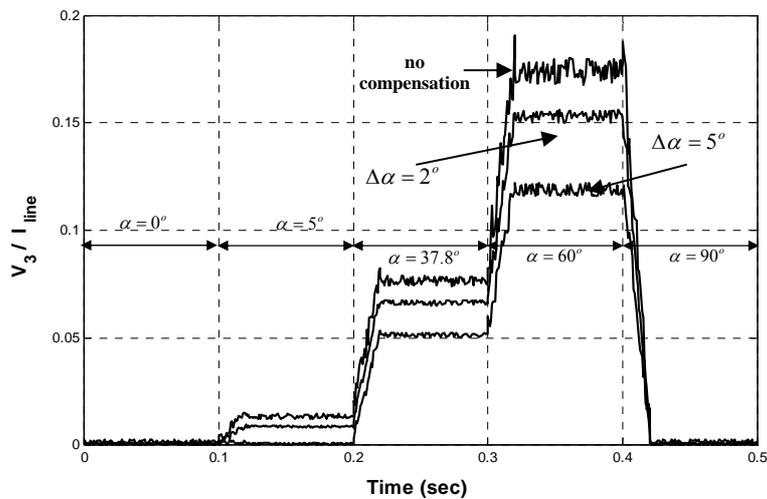


Fig. 8. Simulation results: ratio of third voltage harmonics of TCSC to line current with and without the proposed adaptive $\Delta\alpha$ controller

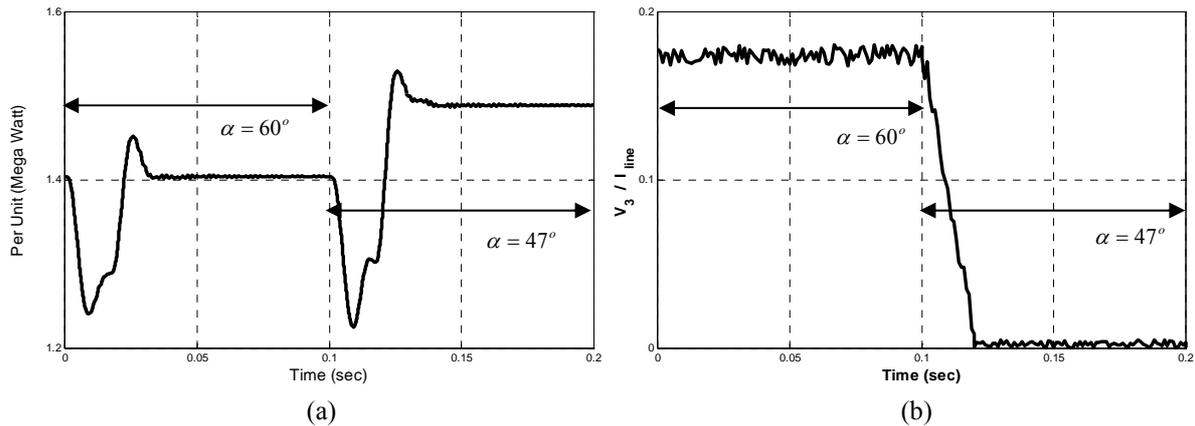


Fig. 9. Transmitted power and harmonics injection of TCSC with the proposed adaptive controller: (a) transmission line sending power; (b) ratio of third harmonic voltage of TCSC to line current

7. CONCLUSION

Harmonic pollutions of TCSCs in compensated transmission lines are investigated. An adaptive firing angle controller capable of limiting TCSC harmonics is proposed. Simulink facilities are used for theoretical analysis and system simulation.

The main conclusions are:

- Harmonic pollutions of TCSC are highly dependent on the firing angle and compensated level (Fig. 5).
- Generated harmonic levels are nonlinear functions of the TCSC component values (Table 2, Fig. 5).
- Decreasing the size of TCSC inductor, rapidly increases the harmonic pollution.
- Harmonic voltages of a TCSC depend on line current (Eq. (6)).
- The proposed adaptive harmonics controller does not have any undesired effects on TCSC characteristics (Fig. 9).
- Implementation of proposed method is relatively simple (Table 3).

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